

Angle of arrival (AOA)-based Cross-localization Algorithm using Orientation Angle for Improved Target Estimation in Far-field Environments

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Abstract — Passive positioning systems with a small aperture array exhibit poor accuracy of target estimation in far-field environments. To improve this accuracy, this paper presents a novel angle-of-arrival (AOA)-based cross-localization algorithm for direction finding using orientation angle. Improved geometric and numerical target-positioning models are constructed after analyzing the mechanism of the conventional AOA-based cross-positioning algorithm. The target predication equation is then derived using the constructed models, and the equation for nonlinear estimation is linearized using the Taylor series. An unbiased estimation of the target is obtained by optimizing the control of the iteration process, thus achieving an accurate positioning of the target. The performance of the proposed algorithm was evaluated in terms of its effectiveness and positioning accuracy under varying signal-to-noise conditions and orientation angle-measurement errors. Simulation results shows that the proposed algorithm is capable of positioning the target effectively, and offers better positioning accuracy than traditional algorithms under conditions of large AOA measurement errors or high-level background noise.

Keywords - Lateral cross localization; Orientation angle; Gauss-Newton iteration; Error characteristics

I. INTRODUCTION

The technology of signal location is widely used in radar, sonar and navigation systems, and can be classified as active or passive location, with different targets. Passive location technology has a broad scope of development and application prospects in military due to its concealed nature [1]. The targets can be positioned by a single receiving node or a multi-node network [2]. In comparison with the single-node localization, the multi-node network has a higher signal gain and target resolution. According to different implementation techniques, the positioning methods mainly include combining the space and time cumulative positioning [3], fusion azimuth and time difference of arrival (TDOA) [4], positioning methods based on Doppler shift [5], multipath target motion analysis (TMA), signal strength, and line spectral characteristics [6,7]. Different monitoring environment and objectives require different positioning methods. For example, the methods that combine azimuth and TDOA are applied in situations where the sensor array aperture is comparable to the target distance; while the time cumulative methods require high-precision time reference, the methods based on azimuth and Doppler shift have high accuracy on high-frequency fast-moving targets [8, 9, 10].

This paper mainly focuses on far-field targeting technology in a small aperture array. By analyzing the characteristics of a far-field signal and a small aperture array, we propose an AOA cross-localization algorithm using signal orientation angle. The algorithm uses multiple AOAs measured by different nodes to locate the target. To deal with the problem of nonlinear estimation, predictive equations are defined and linearized by Taylor series expansion. The parameters are estimated through

Gauss-Newton iteration using maximum likelihood estimation, and the targets' position is then obtained through optimal estimation. The proposed algorithm can improve the positioning accuracy of AOA cross-localization method effectively, especially under significant orientation error and complex background noise.

II. RELATED WORK

The optimal passive targeting method involves centralized global information processing. Each array sends the observed data to the fusion center which estimates the target using the global information. Typical location algorithms based on complete information include least squares algorithm [11], maximum likelihood algorithm [12] and the algorithm based on space-time subspace optimization [13]. Weiss [11] have reported the use of the L -base sensor array to receive radio frequency signal transmitted by a single transmitter, and using least squares method to position the transmitter directly. Through maximizing the eigenvalues of an $L \times L$ matrix, the transmitter location can be obtained with a simply 2-D search algorithm. Another extended single-objective targeting for multiple transmitters positioning has been reported by Weiss *et al.* [11]. Another approach [13] uses the method of maximum likelihood and subspace optimization. The objective functions for the direct position of multiple transmitters include attenuation coefficient, signal source, target position, and other unknown parameters. The maximum likelihood method requires a multi-dimensional search but the subspace optimization method is able to locate all targets with only a two-dimensional search. Methods reported in [11] and [13] have also considered situations where the signal

waveform is known so that the optimization cost can be simplified to varying degrees.

Although the centralized global information processing method is theoretically optimal, its implementation process needs large communication bandwidth, computation, and energy consumption [14]. In practical applications, the positioning system for different scenarios is restricted by energy resources. For example, the positioning nodes deployed in harsh environments are powered by ordinary batteries and are often left unattended; thus, the energy of each node is extremely limited. Besides, to achieve global information by directly targeting the algorithm, each array requires strict time synchronization [15]. For example, the approach in [13] assumes that time synchronization level of each base station before positioning is 50 ns. Such high synchronization accuracy necessitates high demands of hardware and synchronization algorithm.

Under the premise of limited communication bandwidth and energy, researchers have proposed many resource-constrained wireless passive-targeting algorithms. Among these, the most common algorithm is based on azimuth [16, 17]. These algorithms based on azimuth and their corresponding systems have been widely used due to their low resource consumption, and lower hardware and software requirement. Some examples include the Acoustic ENSBox in California Institute of Technology [18–20], VoxNet [21], and array system based on sound propagation delay compensation developed by Kaplan *et al.* [22, 23].

Pure azimuth targeting is a simple and practical closed linear algorithm. The representative linear algorithms mainly include the Stansfield estimator [24] and the orthogonal vector (OV) algorithm [25]. If the weight matrix of the Stansfield estimator is replaced by a unit matrix, the Stansfield estimator becomes equivalent to the OV algorithm. The linear estimator offer advantages of being simple to compute and easy to implement. However, they suffer from limitations of low accuracy and estimator bias. With the increase in observed data, estimation deviation continues to exist and does not reduce. Therefore, a several modifications to address this problem have been reported in literature such as instrumental variable (IV) [26–28], constrained least squares (CLS) [29], and total least squares (TLS) [30, 31]. The IV estimator is consistent, progressive and unbiased. Its root mean-square error (*RMSE*) is progressive and tends towards the Cramer–Rao lower bound (CRLB). Le Cadre and Jauffret proved that the convergence of the IV algorithm is very sensitive to the initial value and the selection of step [32]. Ho *et al.* proposed the CLS algorithm and conducted target motion analysis. The CLS algorithm has been proved to be progressive and unbiased. Gu [33] proved that the CLS algorithm is actually a progressive maximum-likelihood estimator. Similarly, the TLS algorithm is also a progressive maximum-likelihood estimator. CLS is simpler than TLS but it can only be used for a class of pseudo-linear models. By contrast, TLS can be applied to more universal models such as angle observers. It should be noted that at low *SNR*, the

position estimates of both CLS and TLS have a large *RMSE*. Additionally, with less measurement data, CLS serves as the approximation of the OV estimator.

The deviation of closed loop linear estimator can be eliminated by traditional bearing maximum-likelihood (TBML) estimator or nonlinear least squares. Gavish *et al.* [34] pointed out that the *RMSE* of a closed loop linear estimator may be smaller than TBML estimator for limited observation data. When the amount of observation data is large enough, the TBML estimator has a better performance than the closed-loop linear estimator. Assume that the angle observation noise obeys a Gaussian distribution with zero mean; the cost function of the TBML is nonlinear and non-convex. Therefore, the TBML problem is always solved by gradient search such as Newton–Raphson iterative method.

In particular, the IV and numerical TBML iterative algorithms may be divergent under conditions such as poor initial value, fewer observations, or worse geometric positional relationship between target and angle observer. Bishop *et al.* [35] proposed a new algorithm based on Geometry Constrained Least Squares (GCLS) which minimizes the angle observation error under the constraint of geometric positional relationship between the target and angle observer. This method is equivalent to TBML under Gaussian observation noise because the geometric constraints do not provide any additional information to the position estimate. However, the geometric constraints can aid the convergence of the nonlinear least-square algorithm on the basis of angle observation. In comparison with TBML, the GCLS could converge under poor geometric positional relationship between the target and the angle observer; moreover, CLS and TLS are simpler, and more effective with the increase in measurement data and in achieving maximum-likelihood estimation progressively. In the case of large observation error, the estimation accuracy of numerical TBML is higher than CLS and TLS, but the TBML diverges easily or converges only to a local minima in the cases mentioned above.

III. ANGLE OF ARRIVAL (AOA) CROSS-POSITIONING SYSTEM MODEL

A. Description of AOA Cross-positioning Method

The AOA cross-positioning methods estimate targets with the signal AOA obtained by nodes. The positioning accuracy is determined by the direction finding (DF) accuracy of the sensors. Assume that if multiple nodes detect the same target almost at the same time, we can obtain pluralities of the bearing lines [36]. Without loss of generality, we investigate the two-dimensional case first, and then extend the method to three-dimensional space. The measuring principle is shown in Fig. 1.

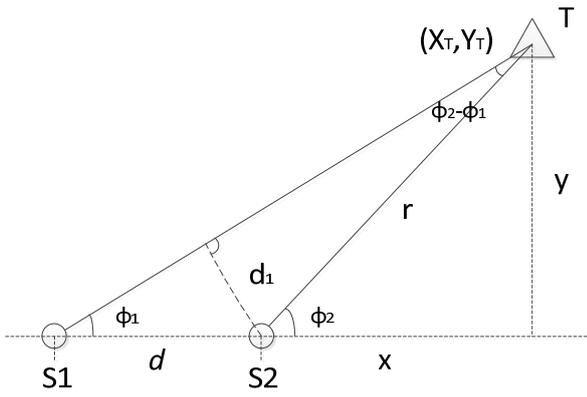


Fig.1 Schematic of AOA cross-positioning

Here S1, S2 are probe nodes, T is target, and the distance between probe nodes is d . Then,

$$\sin \phi_1 = \frac{d_1}{d}, \quad \sin(\phi_2 - \phi_1) = \frac{d_1}{r} \quad (1)$$

Thus,

$$r = \frac{d \sin \phi_1}{\sin(\phi_2 - \phi_1)} \quad (2)$$

Following (1) and (2), and the relationship shown in Fig.1, we obtain:

$$\begin{cases} x = \frac{d \sin \phi_1 \cos \phi_2}{\sin(\phi_2 - \phi_1)} \\ y = \frac{d \sin \phi_1 \sin \phi_2}{\sin(\phi_2 - \phi_1)} \end{cases} \quad (3)$$

The position coordinates of the target can be calculated using (3), and the method is suitable for multiple targets. In practical applications, there are measurement errors and noise in the target AOA that may produce a large deviation between the obtained and the actual position. By increasing the number of nodes, we can obtain more orientation lines and improve the positioning accuracy. With the presence of noise and error, these orientation lines do not always intersect at one point but stagger into an irregular polygon.

We first study three sensor nodes in a two-dimensional plane, where the three orientation lines intersect into a triangle. The position of the target is assumed to be the centroid of the triangle. The number of orientation lines is more than three in a three-dimensional space with a multiple-node array. In order to obtain more accurate results, we can first select three orientation lines to obtain a centroid, and then take the centroid (or mean) of different centroids. This paper mainly focuses on the single target location problem in a three-dimensional space.

B. Targeting Model

Assume the coordinates of target to be estimated is $\mathbf{x}_T = [x_T, y_T, z_T]^T$, the angles measured once by N nodes are $\{u_i, i = 1, 2, \dots, N\}$, where $u_i \in \{\varphi_i, \phi_i\}$, φ_i is the pitch angle, and ϕ_i is the azimuth angle. The schematic diagram is shown in Fig.2. For multiple nodes, set the coordinate

vector as $s_i = [x_i, y_i, z_i]$, the angle u_i can be obtained by the node coordinate values.

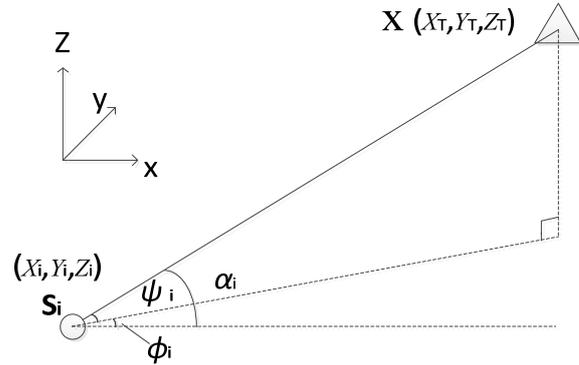


Fig.2 Schematic of orientation cross positioning

Since the measurement system contains additive random error, the system numerical model is always referred to as:

$$u_i = f_i(x_T) + n_i, (i = 1, 2, \dots, N) \quad (4)$$

where N is the number of detection nodes. Expressed in matrix form,

$$\mathbf{u} = f(\mathbf{x}_T) + \mathbf{n} \quad (5)$$

If the measurement results do not contain errors, then $u_i = f_i(x_T) = \alpha_i$ and the relationship between AOA and target coordinates in $f_i(x_T)$ is nonlinear. Assuming that measurement error, n_i , follows the relation:

$$E\{n_i\} = 0, E\{n_i n_j\} = \sigma_{ij} \quad (6)$$

$$\sigma_{ij} = \begin{cases} \sigma_i^2, i = j \\ \rho_{ij} \sigma_i \sigma_j, i \neq j \end{cases} \quad (7)$$

where σ_i and σ_j are standard deviations in i^{th} and j^{th} monitoring experiment, ρ_{ij} is the correlation coefficient between position values. To solve the above nonlinear problem, first we need to linearize the prediction equations. We expand the equations according to Taylor series at reference point \mathbf{x}_{T0} , where $\mathbf{x}_{T0} = [x_{T0}, y_{T0}, z_{T0}]^T$ is the initial estimate. We take the second (or first few order terms) of the expanded series and obtain the fixed initial equation:

$$w_{oi} = u_i + g_{oi}^T x_T, (i = 1, 2, \dots, N) \quad (8)$$

where w_{oi} is the fixed measurement. The calculation formula as following:

$$w_{oi} = u_i + g_{oi}^T x_{T0} - f_{oi}, (i = 1, 2, \dots, N) \quad (9)$$

where g_{oi}^T is the gradient of $f_i(x_T)$ at point x_{T0} . It is defined as:

$$\mathbf{g}_{oi}^T = \left. \frac{\partial f_i(x_T)}{\partial \mathbf{x}_T} \right|_{x_T=x_{T0}} = \left[\frac{\partial f_i(x_T)}{\partial x_T} \quad \frac{\partial f_i(x_T)}{\partial y_T} \quad \frac{\partial f_i(x_T)}{\partial z_T} \right]_{x_T=x_{T0}} \quad (10)$$

where f_{oi} is the value of $f_i(x_T)$ at x_{T0} and $f_{oi} = f_i(x_{T0})$.

The N monitoring nodes have N initial relationships as formula (8); combining them into a matrix:

$$\mathbf{w}_0 = \mathbf{G}_0 \mathbf{x}_T + \mathbf{n} \quad (11)$$

where \mathbf{w}_0 is obtained by the following formula:

$$\mathbf{w}_0 = \mathbf{u} + \mathbf{G}_0 \mathbf{x}_T - \mathbf{f}_0 \quad (12)$$

Here, $\mathbf{w}_0, \mathbf{u}, \mathbf{n}, \mathbf{f}_0$ are $N \times 1$ dimensional column vectors:

$$\mathbf{w}_0 = [w_{01}, w_{02}, \dots, w_{0i}, \dots, w_{0N}]^T \quad (13)$$

$$\mathbf{u}_0 = [u_{01}, u_{02}, \dots, u_{0i}, \dots, u_{0N}]^T \quad (14)$$

$$\mathbf{n}_0 = [n_{01}, n_{02}, \dots, n_{0i}, \dots, n_{0N}]^T \quad (15)$$

$$\mathbf{f}_0 = [f_{01}, f_{02}, \dots, f_{0i}, \dots, f_{0N}]^T \quad (16)$$

\mathbf{G}_0 is an $N \times 3$ dimensional gradient matrix, whose i^{th} row is a 1×3 dimensional gradient vector \mathbf{g}_{oi}^T , or i^{th} column of \mathbf{G}_0^T is a 1×3 dimensional gradient vector \mathbf{g}_{oi} . Therefore,

$$\mathbf{G}_0 = [\mathbf{g}_{01}, \mathbf{g}_{02}, \dots, \mathbf{g}_{0i}, \dots, \mathbf{g}_{0N}]^T \quad (17)$$

where the error vector \mathbf{n} meets the criterion:

$$E\{\mathbf{n}\} = 0, E\{\mathbf{n}\mathbf{n}^T\} = \mathbf{R} \quad (18)$$

in which $\mathbf{R} \in V (N \times N)$ is measurement error covariance matrix, \mathbf{n} is Gaussian random variable. The maximum likelihood estimation $\hat{\mathbf{x}}_T$ of the target position vector \mathbf{x}_T can be solved by Gauss-Newton iterative. The procedure is:

$$\hat{\mathbf{x}}_{T,m+1} = (\mathbf{G}_m^T \mathbf{R}^{-1} \mathbf{G}_m)^{-1} \mathbf{G}_m^T \mathbf{R}^{-1} \mathbf{w}_m, m = 0, 1, 2, \dots \quad (19)$$

where m is the iterations count. $\mathbf{w}_m, \mathbf{G}_m$ are:

$$\mathbf{w}_m = \mathbf{u} + \mathbf{G}_m \hat{\mathbf{x}}_{T,m} - \mathbf{f}_m \quad (20)$$

$$\mathbf{w}_m = \mathbf{u} + \mathbf{G}_m = \left. \frac{\partial f(\mathbf{x}_T)}{\partial \mathbf{x}_T} \right|_{x_T=\hat{x}_{T,m}}, \mathbf{f}_m = f(\hat{\mathbf{x}}_{T,m}) \quad (21)$$

Take $\hat{\mathbf{x}}_{T,m}$ obtained at each iteration as the initial value \mathbf{x}_{T0} for the next iteration. Note that \mathbf{x}_T obtained in initial iteration is $\hat{\mathbf{x}}_{T,1}$. According to (19):

$$\hat{\mathbf{x}}_{T,1} = (\mathbf{G}_0^T \mathbf{R}^{-1} \mathbf{G}_0)^{-1} \mathbf{G}_0^T \mathbf{R}^{-1} \mathbf{w}_0 \quad (22)$$

where $m = 0$. Thus, the target values are a series of revised estimation sequence:

$$\mathbf{x}_{T0}, \hat{\mathbf{x}}_{T,1}, \hat{\mathbf{x}}_{T,2}, \dots, \hat{\mathbf{x}}_{T,m}, \hat{\mathbf{x}}_{T,m+1} \dots \quad (23)$$

If the initial point \mathbf{x}_{T0} of iterative process is near the global minimum point of squared weighted cost function as following:

$$S(\mathbf{x}_T) = \mathbf{n}^T \mathbf{R}^{-1} \mathbf{n} = [\mathbf{u} - f(\mathbf{x}_T)]^T \mathbf{R}^{-1} [\mathbf{u} - f(\mathbf{x}_T)] \quad (24)$$

and satisfies the iteration convergence conditions, then the final estimates are given as:

$$\hat{\mathbf{x}}_T = \lim_{m \rightarrow \infty} \hat{\mathbf{x}}_{T,m} \quad (25)$$

In practical applications, the commencement and termination of the iterative process is controlled by a threshold, and we study these guidelines in the following algorithm.

IV. PROPOSED AOA CROSS-LOCALIZATION ALGORITHM USING ORIENTATION ANGLE

A. Description of the Proposed Algorithm

For the targeting-related issues in a three-dimensional space, we study the orientation angle α on the basis of azimuth and pitch angle, as shown in Fig.2. The relationship between α and ϕ, φ is:

$$\alpha = \arctan \sqrt{\tan^2 \varphi + \tan^2 \phi} \quad (26)$$

or

$$\alpha = \arccos \sqrt{\cos \varphi \cos \phi} \quad (27)$$

Then for i^{th} node $s_i = [x_i, y_i, z_i]$, $i = 1, 2, \dots, N$, the relationship with target $\mathbf{x}_T = [x_T, y_T, z_T]^T$ is:

$$f_i(\mathbf{x}_T) = \alpha_i = \arctan \frac{\sqrt{(x_T - x_i)^2 + (z_T - z_i)^2}}{y_T - y_i} \quad (28)$$

When the number of iteration is m , the gradient vector is:

$$\mathbf{g}_{mi} = \left[\frac{\hat{x}_m - x_i}{r_{mi}^2 s_{mi}} \quad -\frac{\hat{y}_m - y_i}{r_{mi}^2 s_{mi}} \quad \frac{\hat{z}_m - z_i}{r_{mi}^2 s_{mi}} \right]^T \quad (29)$$

where

$$r_{mi}^2 = (\hat{x}_m - x_i)^2 + (\hat{y}_m - y_i)^2 + (\hat{z}_m - z_i)^2 \quad (30)$$

$$s_{mi} = \sqrt{\left(\frac{r_{mi}}{\hat{y}_m - y_i}\right)^2 - 1} \quad (31)$$

The N gradient vectors constitute a gradient matrix:

$$\mathbf{G}_m = [\mathbf{g}_{m1}, \mathbf{g}_{m2}, \dots, \mathbf{g}_{mN}]^T \quad (32)$$

The covariance matrix of orientation angle error in m^{th} iteration is an $N \times N$ dimensional diagonal matrix. Diagonal elements of the matrix vary with the iterative equation, which is:

$$\mathbf{R}_m = \text{diag}[\sigma_{m1}^2, \sigma_{m2}^2, \dots, \sigma_{mN}^2]^T \quad (33)$$

where σ_{mi}^2 is error variance of orientation angle in m^{th} iteration. The solution is:

$$\sigma_{mi}^2 = a_{mi}\sigma_{\phi_i}^2 + b_{mi}\sigma_{\phi_i}^2 + c_{mi}\rho_i\sigma_{\phi_i}\sigma_{\phi_i} \quad (34)$$

where

$$a_{mi} = \left(\frac{1}{s_{mi}} \frac{\hat{x}_m - x_i}{\hat{y}_m - y_i} \right)^2 \quad (35)$$

$$b_{mi} = \left\{ s_{mi} \left[\left(\frac{r_{mi}}{\hat{z}_m - z_i} \right) - 1 \right]^{1/2} \right\}^{-2} \quad (36)$$

$$c_{mi} = \sqrt{a_{mi}b_{mi}} \quad (37)$$

Assume that the ambient noise is additive Gaussian white noise, the iterative equation can be expressed as:

$$\hat{\mathbf{x}}_{T,m+1} = (\mathbf{G}_m^T \mathbf{R}_m^{-1} \mathbf{G}_m)^{-1} \mathbf{G}_m^T \mathbf{R}_m^{-1} \mathbf{w}_m \quad (38)$$

where

$$\mathbf{w}_m = \mathbf{u} + \mathbf{G}_m \hat{\mathbf{x}}_{T,m} - f(\hat{\mathbf{x}}_{T,m}) \quad (39)$$

in which $f(\hat{\mathbf{x}}_{T,m})$ is the value of $f(\mathbf{x}_T)$ at $\mathbf{x}_T = \hat{\mathbf{x}}_{T,m}$.

B. Iterative Process Control

For the iterative process, we need to first analyze the value of initialization estimate \mathbf{x}_{T0} of position vector \mathbf{x}_T . The value methods of \mathbf{x}_{T0} mainly include experience speculation and rough calculation on measurements. Here, the initialization estimate is received through solving the intersection of a group of AOA in observation surface.

Assume AOA of a set of known measurements $\{\varphi_i, \varphi_j, \phi_k\}$ that intersect at point \mathbf{x}_{ijk} , such that $i \neq j$ and $k = i, j$ or $k \neq i, j$. The intersection point can be determined by the equation set below:

$$\begin{cases} \varphi_i = \arctan \frac{x - x_i}{y - y_i} \\ \varphi_j = \arctan \frac{x - x_j}{y - y_j} \\ \phi_k = \arctan \frac{z - z_j}{\sqrt{(x - x_j)^2 + (y - y_j)^2}} \end{cases} \quad (40)$$

Solution of the equation can be expressed as:

$$\mathbf{x}_{ijk} = [x_{ij} \ y_{ij} \ z_{ijk}]^T \quad (41)$$

where

$$\begin{cases} x_{ij} = \frac{(y_i - y_j)a_{ij} + x_j a_{ij} + x_i d_{ij}}{\sin(\varphi_i - \varphi_j)} \\ y_{ij} = \frac{(x_i - x_j)b_{ij} + y_j c_{ij} + y_i d_{ij}}{\sin(\varphi_i - \varphi_j)} \\ z_{ijk} = z_k + \sqrt{(x_{ij} - x_k)^2 + (y_{ij} - y_k)^2} \tan \phi_k \end{cases} \quad (42)$$

By analysis of the target space, we obtain:

$$\begin{cases} a_{ij} = \sin \varphi_i \sin \varphi_j \\ b_{ij} = \cos \varphi_i \cos \varphi_j \\ c_{ij} = \sin \varphi_i \cos \varphi_j \\ d_{ij} = \cos \varphi_i \sin \varphi_j \end{cases} \quad (43)$$

Here, \mathbf{x}_{ijk} is initialization priori information, that is:

$$\mathbf{x}_{T0} = \mathbf{x}_{ijk} \quad (44)$$

For iterative process control, the threshold should satisfy some criterion of positioning accuracy:

$$D(\Delta \hat{\mathbf{x}}_{T,m}) = \begin{cases} A, & (\Delta \hat{\mathbf{x}}_{T,m})^T \Delta \hat{\mathbf{x}}_{T,m} \leq \zeta^2 \\ B, & (\Delta \hat{\mathbf{x}}_{T,m})^T \Delta \hat{\mathbf{x}}_{T,m} > \zeta^2 \end{cases} \quad (45)$$

where D is control instruction, A and B are the termination and continuation of the iterative process respectively, ζ is the estimation accuracy, $\Delta \hat{\mathbf{x}}_{T,m}$ is the difference between two estimated values:

$$\Delta \hat{\mathbf{x}}_{T,m} = \hat{\mathbf{x}}_{T,m+1} - \hat{\mathbf{x}}_{T,m} \quad (46)$$

C. Analysis of Estimation Error

An error in location refers to the deviation between the estimated value $\hat{\mathbf{x}}_T$ and actual value \mathbf{x}_T of the target position. After the $(m + 1)^{\text{th}}$ iteration, the error vector covariance matrix of the position vector \mathbf{x}_T is:

$$\mathbf{R}_{\hat{\mathbf{x}}_{T,m+1}} = (\mathbf{G}_m^T \mathbf{R}_m^{-1} \mathbf{G}_m)^{-1} \quad (47)$$

where \mathbf{R}_m is the covariance matrix of the pre-observation estimation error for describing the error in position estimation.

This algorithm locates the target based on AOA obtained by sensor nodes. The influence on positioning is due to various factors such as measurement error and noise, and concentrated expression in orientation angle error. For the positioning system shown in Fig.2, assume there exist Gaussian white noise n_k with zero mean and variance σ_n^2 , deviation ϕ with zero mean and variance σ_ϕ^2 .

We can get:

$$E\{n_i n_k\} = \sigma_n^2 \delta_{jk} \quad (48)$$

The observations of orientation angle are:

$$\phi_k = \arctan\left(\frac{\Delta y_k}{\Delta x_k}\right) + \phi + n_k, \quad k = 1, 2, \dots, N \quad (49)$$

where $\Delta y_k = y_T - y_k$, $\Delta x_k = x_T - x_k$. Define $\boldsymbol{\theta} = [x_T, y_T, \phi]^T$ as the estimate vector. Here, $\boldsymbol{\theta}$ obeys the multidimensional normal distribution with mean vector, \mathbf{m} , and positive definite covariance matrix $\boldsymbol{\Sigma}$. Define $h(\mathbf{m}, \boldsymbol{\theta}) = \mathbf{0}$ as constraint vector, and

$$\mathbf{h}_m = \frac{\partial h}{\partial \mathbf{m}}, \quad h_\theta = \frac{\partial h}{\partial \boldsymbol{\theta}} \quad (50)$$

For vector $\boldsymbol{\theta}$ with predict prior information, its CRLB is:

$$\mathbf{S}_\theta = \left[\mathbf{h}_\theta^T (\mathbf{h}_m \boldsymbol{\Sigma} \mathbf{h}_m^T)^{-1} \mathbf{h}_\theta + \mathbf{J} \right]^{-1} \quad (51)$$

Assume variance σ_ϕ^2 of deviation is known and is non-zero, then

$$\mathbf{J} = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 1/\sigma_\phi^2 \end{bmatrix} \quad (52)$$

Differentiate formula (49) on the estimator $\boldsymbol{\theta}$, then

$$\mathbf{h}_\theta = [\mathbf{G} \quad \mathbf{I}_N] \quad (53)$$

where

$$\mathbf{G} = \begin{bmatrix} -\frac{\Delta y_1}{r_1^2} & -\frac{\Delta y_2}{r_2^2} & \dots & -\frac{\Delta y_N}{r_N^2} \\ -\frac{\Delta x_1}{r_1^2} & -\frac{\Delta x_2}{r_2^2} & \dots & -\frac{\Delta x_N}{r_N^2} \end{bmatrix}^T \quad (54)$$

$$r_k^2 = \Delta_{xk}^2 + \Delta_{yk}^2, \quad k = 1, 2, \dots, N \quad (55)$$

\mathbf{I}_N is a vector consisting of $N - 1$ elements; \mathbf{h}_m and $\sigma^{-2} \boldsymbol{\Sigma}$ are $N \times N$ dimensional unit matrix as the noise covariance matrix satisfies the diagonal structure.

$$\begin{aligned} \mathbf{S}_\theta &= \left[[\mathbf{G} \quad \mathbf{I}_N]^T (\sigma_n^2 \mathbf{I}_N)^{-1} [\mathbf{G} \quad \mathbf{I}_N] + \text{diag}(0, 0, \sigma_\phi^{-2}) \right]^{-1} \\ &= \sigma_\phi^2 \left[\begin{array}{cc} \mathbf{V}^{-1} & \mathbf{f} \\ \mathbf{f}^T & (\sigma_n / \sigma_\phi)^2 + \mathbf{N} \end{array} \right]^{-1} \end{aligned} \quad (56)$$

where $\mathbf{f} = \mathbf{G}^T \mathbf{I}_N$, $\mathbf{V} = (\mathbf{G}^T \mathbf{G})^{-1}$. The upper left corner 2×2 subarray of \mathbf{S}_θ is the target estimation CRLB. Inverting the partitioned matrix:

$$\mathbf{S}_\theta = \sigma_n^2 \left(\mathbf{V} + \frac{\mathbf{V} \mathbf{f} \mathbf{f}^T \mathbf{V}}{(\sigma_n / \sigma_\phi)^2 + \mathbf{N} - \mathbf{f}^T \mathbf{V} \mathbf{f}} \right) \quad (57)$$

Since the *priori* bias may be infinite, we get:

$$\mathbf{S}_{\max} = \lim_{\sigma_\phi \rightarrow \infty} \mathbf{S}_\theta = \sigma_n^2 \left(\mathbf{V} + \frac{\mathbf{V} \mathbf{f} \mathbf{f}^T \mathbf{V}}{\mathbf{N} - \mathbf{f}^T \mathbf{V} \mathbf{f}} \right) \quad (58)$$

Here, $\mathbf{S}_\theta \leq \mathbf{S}_{\max}$ shows the influence of deviation with prior information. The error range is defined as:

$$\mathbf{S}_\theta = \sigma_n^2, \quad \sigma_\phi \rightarrow 0 \quad (59)$$

V. SIMULATION AND ANALYSIS

We analyze the performance of the proposed algorithm through simulations. Positioning methods using AOA cross mainly include direct measurement, least squares and their extensions. We compare the performance of the direct AOA cross-localization algorithm (**algorithm 1**), linear least-squares localization algorithm (**algorithm 2**), and the proposed AOA cross-localization algorithm based on orientation angle (**algorithm 3**).

The number of Monte Carlo simulation run time is $N = 5000$. The localization precision is expressed in terms of *RMSE* as:

$$RMSE(u) = \frac{\sum_{i=1}^N \|u^{(i)} - u\|}{N} \quad m \quad (60)$$

where $u^{(i)}$ is the i^{th} target estimation, and the environmental noise is assumed to have a Gaussian distribution. We investigate how the localization precision changes with orientation angle measurement error and *SNR*. The nodes position (in m) are set as $s_1(0, 0, 0)$, $s_2(20, 0, 0)$, $s_3(26, 15, 0)$, $s_4(37, -10, 8)$, $s_5(60, 20, -20)$, and the target position is set as $T(800, 800, 400)$.

A. Algorithm Effectiveness

We locate the target once with different algorithms to test the effectiveness of the single-positioning experiment. Here *SNR* = 10 dB and the positional deviation results are shown in Table I.

TABLE I. COMPARISON OF TARGETING RESULTS FROM DIFFERENT ALGORITHMS

Algorithm	Absolute deviation of estimated position (m)		
	x	y	z
Algorithm 1	1.9	2.1	0.8
Algorithm 2	1.4	1.5	0.7
Algorithm 3	0.6	0.8	0.2

As displayed the Table 1, under the same simulation environment, all the three algorithms are able to locate the target. The positional deviations of different algorithms on the three axes have a significant proportional relationship with the distance of the observation node from the target in that axis. Comparing with algorithm 1 and algorithm 2, algorithm 3 has a smaller deviation, which shows algorithm 3 has better positioning accuracy.

B. Algorithm Performance in Different Orientation Angle Measurement Error

We analyze how the positioning accuracy changes with the gain of orientation angle-measurement error. The number of nodes is five, and the *SNR* is fixed at 0 dB and

10 dB.

Experiment 1: When $SNR = 10$ dB, the RMSE changes with orientation angle-measurement error through 5000 Monte Carlo simulations are shown in Fig.3.

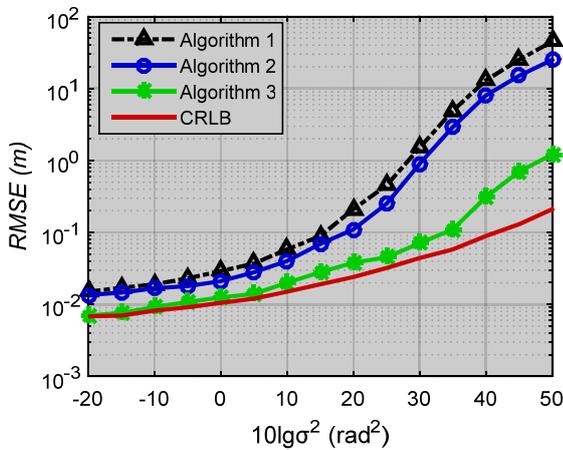


Fig. 3 RMSE curve with orientation angle measurement error for different algorithms at $SNR = 10$ dB

The single solid curve in Fig. 3 is CRLB. The positioning accuracy of three algorithms is close to CRLB when the orientation angle-measurement error is small, and algorithm 3 performs slightly better than algorithm 1 and algorithm 2. With the gain of orientation angle-measurement error, the $RMSE$ of algorithm 1 and algorithm 2 increase significantly, while algorithm 3 continues to have a smaller $RMSE$. This shows that algorithm 3 still possesses a high positioning accuracy with large errors, and greater the error, more obvious is the advantage.

Experiment 2: When $SNR = 0$ dB, the change in $RMSE$ with orientation angle-measurement error in same conditions is shown in Fig.4.

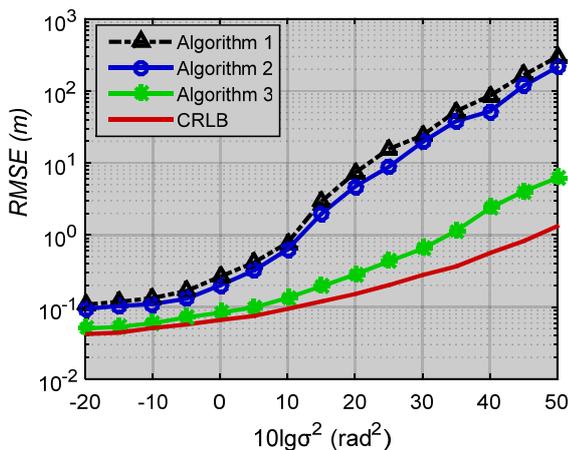


Fig. 4 RMSE curve change with orientation angle-measurement error for different algorithms at $SNR = 0$ dB

Comparing Fig. 4 with Fig. 3, when the SNR is reduced, the three algorithms are still able to locate the target but with a declining accuracy. The comparison between

algorithms shows that the positioning accuracy of algorithm 3 is obviously better than algorithm 1 and 2 when the orientation angle-measurement error increases, and the greater the error, the more obvious is the advantage. Simulations show that the proposed algorithm (3) can still estimate the target accurately despite large orientation angle-measurement error.

C. Performance for varying SNR

To analyze the effect of gain in SNR on positioning accuracy when the orientation angle-measurement error is fixed, we change the SNR from -25 dB to 35 dB, the results of which are shown in Fig.5.

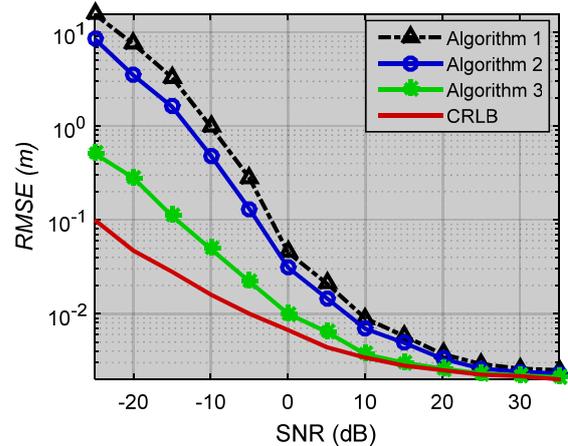


Fig. 5 RMSE change with SNR for different algorithms

As is shown in Fig.5, when the SNR is low, the positioning results of all the three algorithms display a larger deviation, and even worse for algorithms 1 and 2. With the increase in SNR , all the positioning accuracy of all the algorithms improves. Algorithm 3 approaches CRLB when the SNR reaches 10 dB, while algorithm 1 and 2 do not approach CRLB until SNR reach 25 dB. When the SNR is greater than 30 dB, all the three algorithms exhibit similar targeting results. Simulations show that the proposed algorithm is more accurate than the traditional methods under low SNR conditions.

VI. CONCLUSION

In this paper, we proposed an AOA cross-localization algorithm using orientation angle. The algorithm can address targeting problems such as poor resolution, low accuracy under large orientation-angle error, and background noise in far-field environment of traditional algorithms. We constructed the estimation prediction equations with the AOA cross-positioning system geometry model and the numerical model. Progressive unbiased estimate of the target was obtained an iterative process control of the prediction equations. A large number of simulations verified that the proposed algorithm has a smaller location $RMSE$ under different orientation-angle error values and SNR , and the proposed approach displays remarkable potential for engineering applications.

CONFLICT OF INTEREST

The authors declare that there is no conflict of interests regarding the publication of this paper.

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